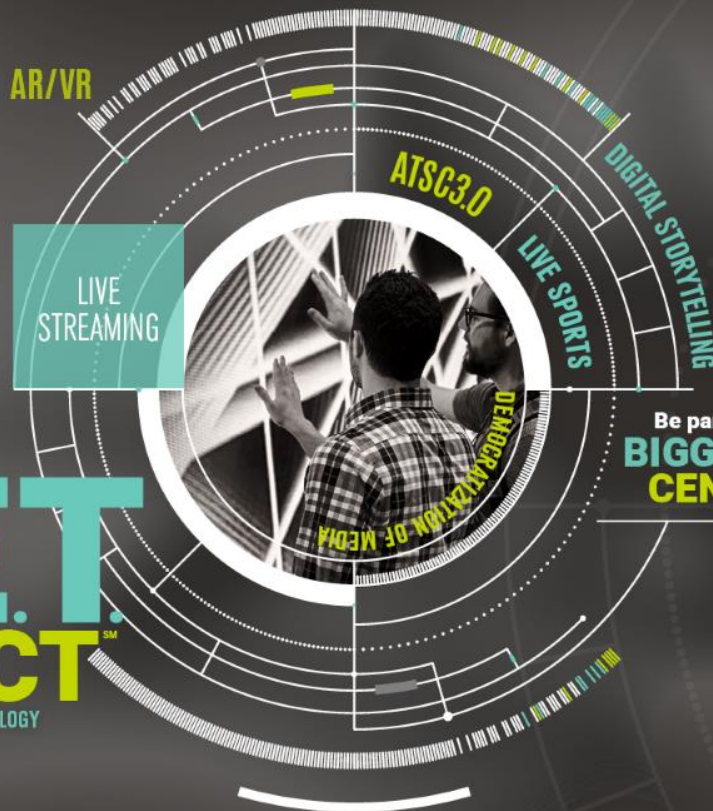


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# ATSC 3.0 – Boosting the Signal Strength - MISO

John L. Schadler



Continuation

“Antenna Technology For ATSC 3.0 – Boosting the Signal Strength”

# More, More, More



Fundamentally changing the way U.S. Broadcast TV is delivered.

Merging internet with broadcast with

- More flexibility
- More services
- More robust delivery
- More platforms



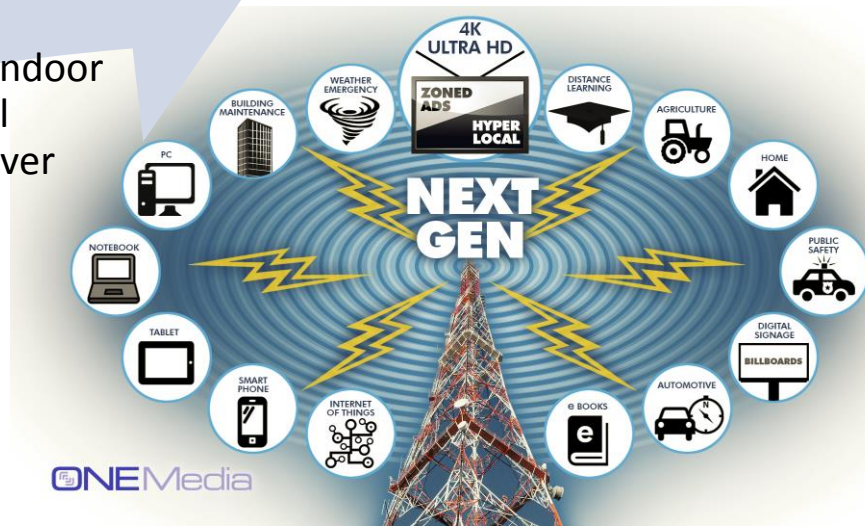
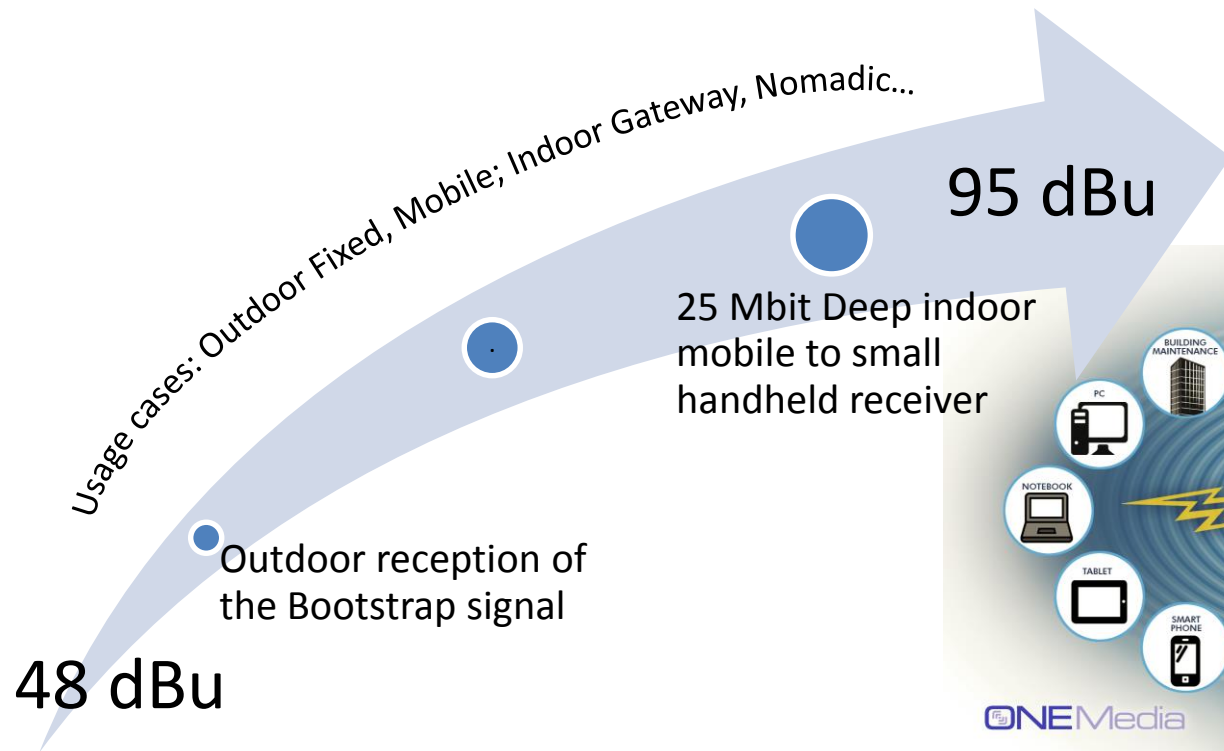
*More bits to  
more places*



*More signal  
strength*

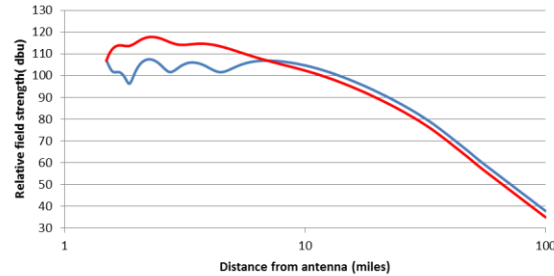
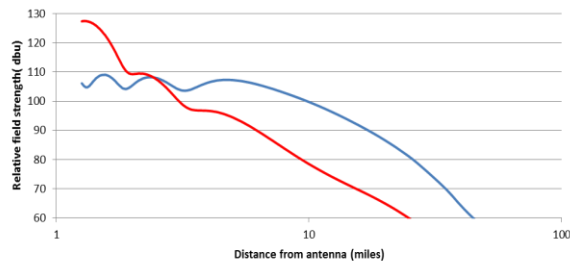
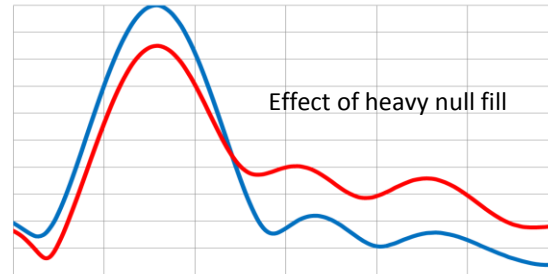
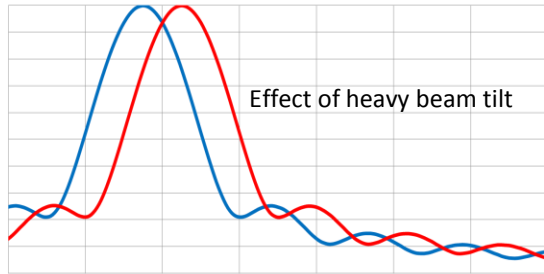


# How much signal strength is required?

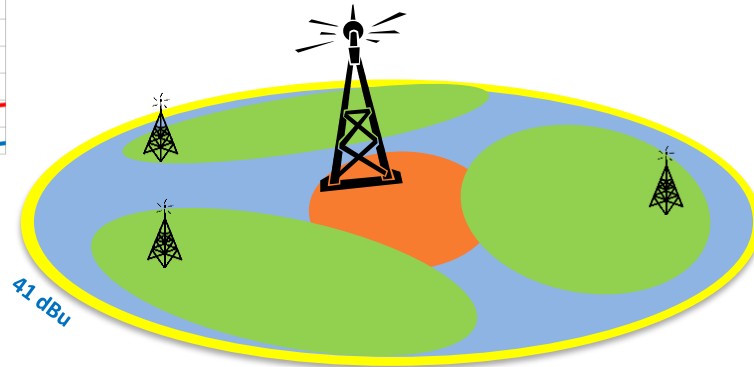


# Review

- ~~1. Increase transmitter power~~
2. Increase beam tilt
3. Increase null fill
4. Add a SFN



## Addition of SFNs

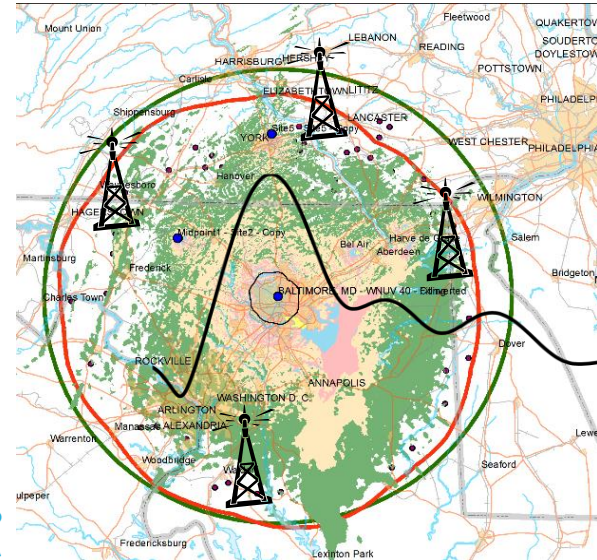


# Review

Most effective way to design for service and provide even distribution of high signal strength – High null fill + SFNs

- Saturate in the vicinity of the main antenna by increasing the null fill
- Add SFN sites around coverage perimeter to boost the signal strength outside of the high null fill area

“FutureFill” + SFN



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# Today

## Boosting the signal strength with MISO diversity

- ATSC 3.0 MISO scheme – TDCFS
  - Transmitting two uncorrelated signals to a single receiver
  - Cost effective
    - Increase the complexity of the transmitter – not the receiver
      - ATSC 3.0 SFN sites will serve many receivers
        - Economical to add equipment cost at the transmit site rather than the receiver
        - Receiver remains small and affordable

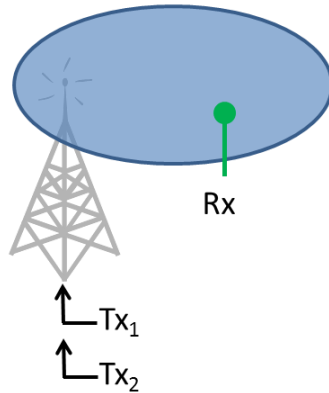


# MISO deployment

- TDCFS can be deployed in either a co-located or distributed configuration

## Co-located

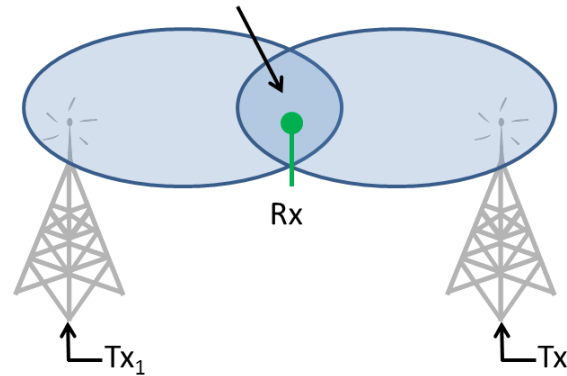
Diversity gain throughout



- Diversity gain throughout the coverage area

## Distributed

Diversity gain in overlap area



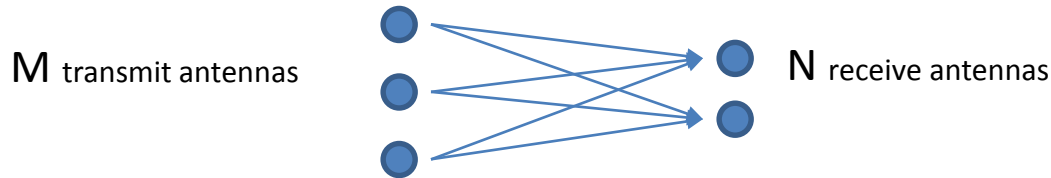
- Does not require any new RF equipment within the existing SFN



# Boosting the signal strength – Diversity gain

Diversity gain  $\equiv$  Boosting the RSS

Max diversity gain is based on the total number of independent signal paths

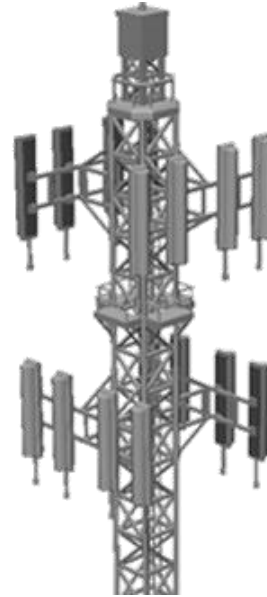


$$1 \leq G_d \leq G_{max} = M * N$$

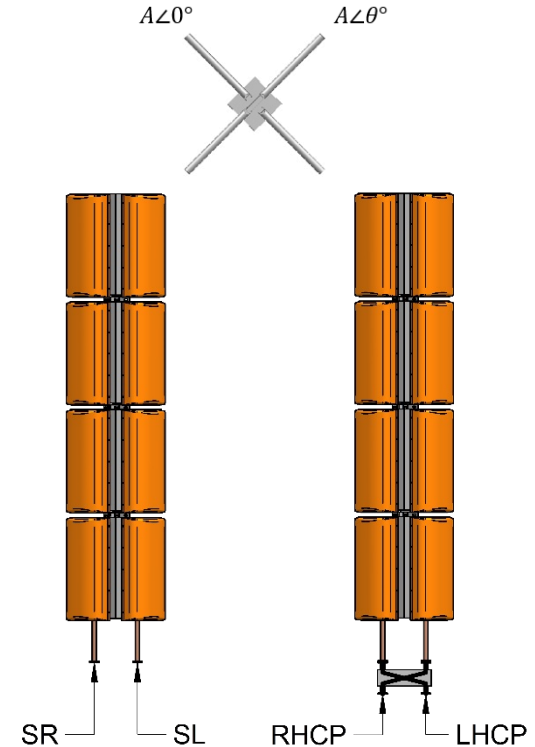
3 dB improvement in RSS can be achieved when 2 x 1 MISO diversity is applied

# Co-located Diversity Implementation

- Traditionally
  - Spatial diversity
    - Separate antennas
    - Difficult to implement
      - Space limitations
  - Polarization diversity
    - Co-located antenna elements
    - Orthogonal polarizations
    - Modes of operation
      - Slant linear
      - RH / LH CP



Dual input broadcast antenna array



Which mode of polarization diversity operation is best for ATSC 3.0 MISO?

# Polarization diversity – Figure of Merit

- Max diversity gain depends on spreading the power evenly between the polarizations
- Figure of merit
  - Cross Polarization Discrimination (XPD)
    - The ratio between the available power in the vertical and horizontal polarizations

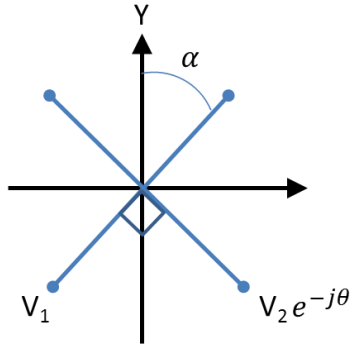
$$XPD = \frac{\langle |R_v|^2 \rangle}{\langle |R_h|^2 \rangle}$$

For optimal diversity gain XPD=0dB

Compare the static response XPD for slant linear and RH/LH CP

# Transmission Channel

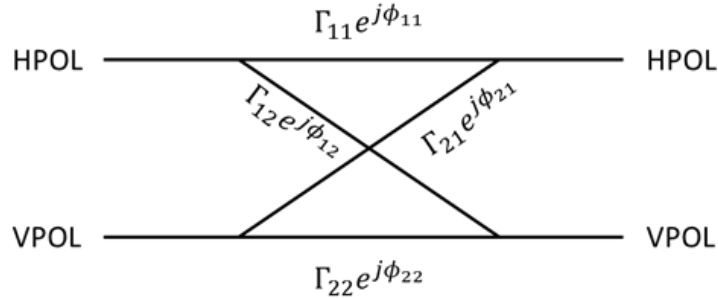
Dipole modeling



Pair of orthogonal crossed dipoles oriented in space by a tilt angle  $\alpha$

$$\begin{pmatrix} V_h \\ V_v \end{pmatrix} = \begin{bmatrix} \sin\alpha & -\cos\alpha \\ \cos\alpha & \sin\alpha \end{bmatrix} \begin{pmatrix} V_1 \\ V_2 e^{-j\theta} \end{pmatrix}$$

Channel modeling



$\Gamma$  – random variable used to model the multipath fading

$\Phi$  – random phase introduced by the channel

Four channel links between the transmitter and receiver

$$\begin{pmatrix} R_h \\ R_v \end{pmatrix} = \begin{bmatrix} \Gamma_{11}e^{j\phi_{11}} & \Gamma_{12}e^{j\phi_{12}} \\ \Gamma_{21}e^{j\phi_{21}} & \Gamma_{22}e^{j\phi_{22}} \end{bmatrix} \begin{pmatrix} V_h \\ V_v \end{pmatrix}$$

# Cross Polarization Discrimination

$$XPD = \frac{\left\langle \frac{V_1^2 [\Gamma_{21}^2 \sin^2 \alpha + \Gamma_{22}^2 \cos^2 \alpha + 2\Gamma_{21}\Gamma_{22} \sin \alpha \cos \alpha \cos(\phi_{21} - \phi_{22})] + V_2^2 [\Gamma_{22}^2 \sin^2 \alpha + \Gamma_{21}^2 \cos^2 \alpha + 2\Gamma_{21}\Gamma_{22} \sin \alpha \cos \alpha \cos(\phi_{21} - \phi_{22})]}{+2V_1V_2 \cos \theta [\Gamma_{21}\Gamma_{22}(\sin^2 \alpha - \cos^2 \alpha) \cos(\phi_{21} - \phi_{22}) + (\Gamma_{22}^2 - \Gamma_{21}^2) \sin \alpha \cos \alpha]} \right\rangle}{\left\langle \frac{V_1^2 [\Gamma_{11}^2 \sin^2 \alpha + \Gamma_{12}^2 \cos^2 \alpha + 2\Gamma_{11}\Gamma_{12} \sin \alpha \cos \alpha \cos(\phi_{11} - \phi_{12})] + V_2^2 [\Gamma_{12}^2 \sin^2 \alpha + \Gamma_{11}^2 \cos^2 \alpha + 2\Gamma_{11}\Gamma_{12} \sin \alpha \cos \alpha \cos(\phi_{11} - \phi_{12})]}{+2V_1V_2 \cos \theta [\Gamma_{11}\Gamma_{12}(\sin^2 \alpha - \cos^2 \alpha) \cos(\phi_{11} - \phi_{12}) + (\Gamma_{12}^2 - \Gamma_{11}^2) \sin \alpha \cos \alpha]} \right\rangle}$$

The definition yields

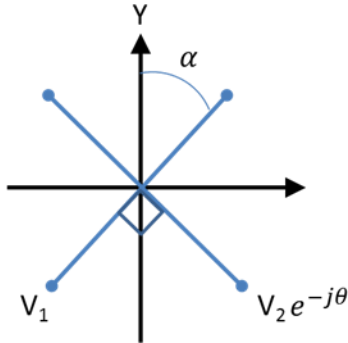
$$XPD = \frac{\langle |R_v|^2 \rangle}{\langle |R_h|^2 \rangle} = \frac{A \langle \Gamma_{21}^2 \rangle + B \langle \Gamma_{22}^2 \rangle}{A \langle \Gamma_{11}^2 \rangle + B \langle \Gamma_{12}^2 \rangle}$$

where

$$A = V_1^2 \sin^2 \alpha + V_2^2 \cos^2 \alpha - 2V_1V_2 \sin \alpha \cos \alpha \cos \theta$$

$$B = V_1^2 \cos^2 \alpha + V_2^2 \sin^2 \alpha + 2V_1V_2 \sin \alpha \cos \alpha \cos \theta$$

The different types of polarization diversity can be described by the coefficients A and B



Polarization	V1	V2	$\alpha$	$\theta$	A	B
Slant Left	1	0	-45	0	0.5	0.5
Slant Right	1	0	45	0	0.5	0.5
RHCP (Slant 45)	0.707	0.707	45	90	0.5	0.5
LHCP (Slant 45)	0.707	0.707	45	-90	0.5	0.5
RHCP (H/V)	0.707	0.707	0	90	0.5	0.5
LHCP (H/V)	0.707	0.707	0	-90	0.5	0.5

# Dual Polarization Slant Linear or CP for ATSC 3.0 MISO?

Since the A and B coefficients are the same in all 6 cases, the equations that describe the XPD are identical in all 6 cases

Slant linear and circularly polarized antennas transmit the same average performance in a static MISO system. The expected diversity gain of SL / SR linear and RH / LH CP are on average the same.

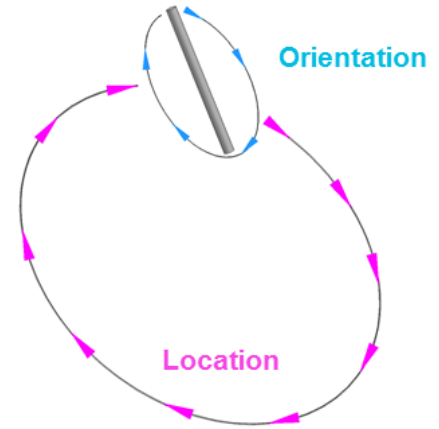
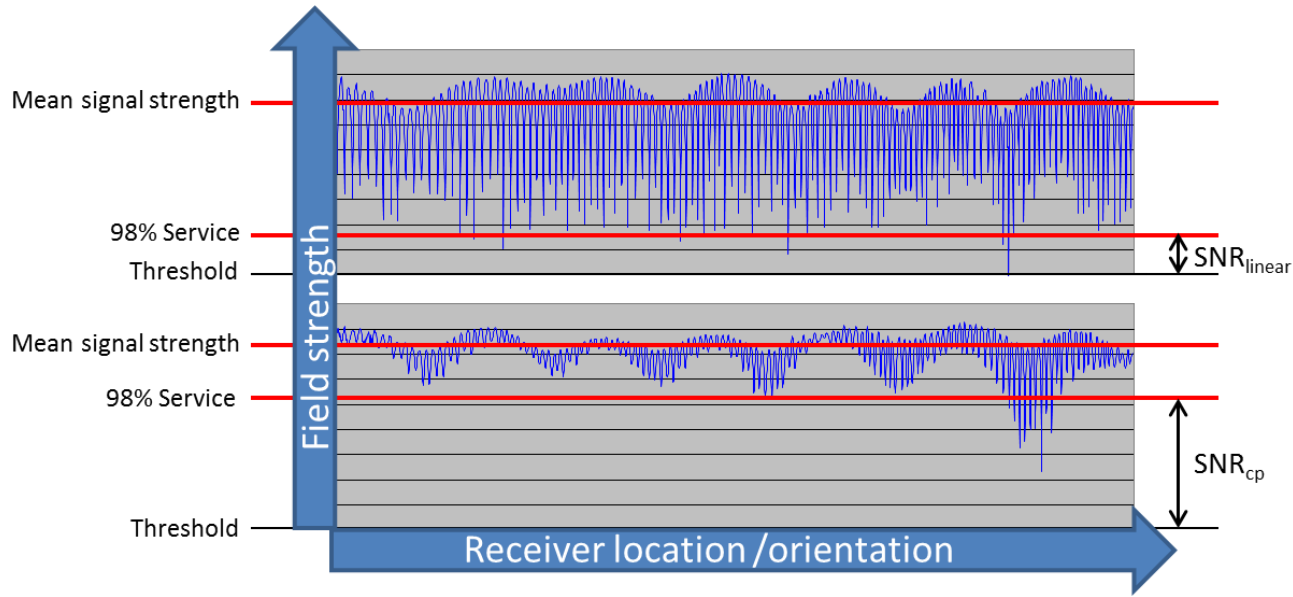


# Dual Polarization Slant Linear or CP for ATSC 3.0 MISO?

- Analysis assumes
  - For CP we increased the transmitter power 3dB to maintain the same ERP
  - The receiver is stationary
  - Independent of any margin improvement observed by transmitting CP to a linearly polarized receive antenna in motion



# What is Margin Improvement?



$$MI = SNR_{cp} - SNR_{linear}$$



# Margin Improvement with Circular Polarization

Starting over a decade ago – extensive testing to quantify the benefit of transmitting CP to a linearly polarized receiver in motion

- Controlled environments
- Field tests in ME and FL
- Indoor / Outdoor / Vehicle
- Measurements based on RSS and BER
- Different amounts of VPOL



# Margin Improvement with Circular Polarization

All measurements have confirmed that transmitting circular polarization to a linearly polarized receiver in motion in a heavy scatter environment provides 5 to 7 dB of margin improvement (MI) over transmitting a linearly polarized signal to the same receiver.



# Margin Improvement and Diversity Gain

- $G_d$  and MI are independent
  - 5-7dB MI is observed when transmitting a single CP signal to a linear receiver in motion
  - Adding a second independent path (MISO) does not change this but adds 3dB of  $G_d$

The total system gain of dual RH / LH CP MSIO diversity system transmitting to a linearly polarized mobile receiver in motion in a heavy scatter environment is as high as 8-10dB.

# Cross Polarization Isolation

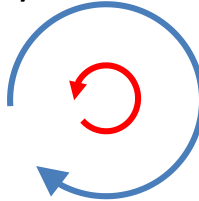
- A new antenna specification to consider
- So far we have assumed the transmit signals are completely uncorrelated
- Imperfect antennas couple energy

SR/SL Linear



$$I = f(\text{cross polarization})$$

RH/LH circular



$$I = f(\text{axial ratio})$$

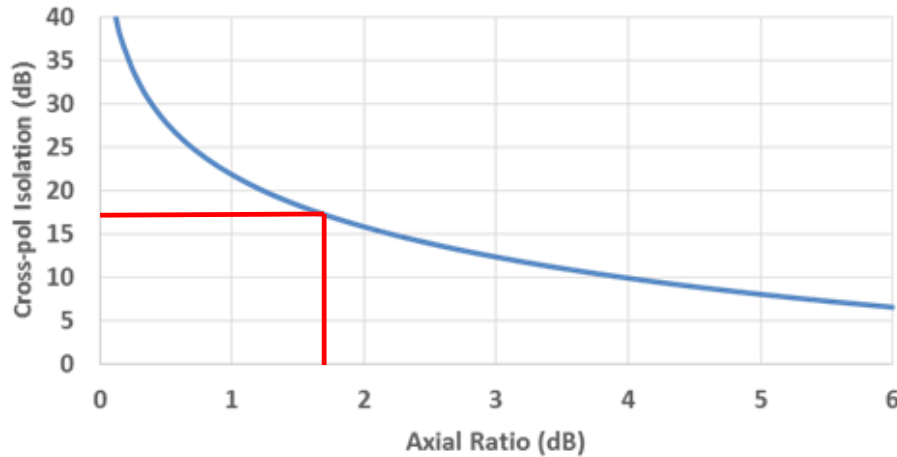
All waves can be decomposed into two components with orthogonal polarization states

- Studies : 17 dB of cross pol isolation is sufficient to reach 99% of desired data rate

# Isolation Between Polarizations for CP Antenna

$$I = 10 \log \left[ \frac{\frac{1}{2} + \frac{AR}{AR^2 + 1}}{\frac{1}{2} \left( \frac{1}{\left( \frac{AR + 1}{AR - 1} \right)^2 + 1} \right) + \frac{AR}{AR^2 + 1} \left( \frac{1}{\left( \frac{AR + 1}{AR - 1} \right)^2 - 1} \right)} \right]$$

Axial Ratio vs. Cross-pol Isolation



Specification  
AR < 1.7 dB for RH/LH CP MISO

# Conclusion

- Employing MISO diversity gain can add up to 3 dB in the system gain
- On average slant linear and circularly polarized antennas transmit the same average performance in a stationary MISO diversity system
- This is independent of any margin improvement observed by transmitting CP to a linearly polarized receive antenna in motion
- Transmitting CP to a linearly polarized receiver in motion in a heavy scatter environment can add 5 to 7 dB of margin improvement
- Total ATSC 3.0 system gains employing RH/LH CP diversity can be 8 to 10dB if you choose to increase your TPO by 3dB.
- The axial ratio specification of a RH / LH co-located system considered for diversity should be  $< 1.7\text{dB}$ .

*\* The use of LH CP will require an FCC rule change*

# Thank you

## Questions?



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